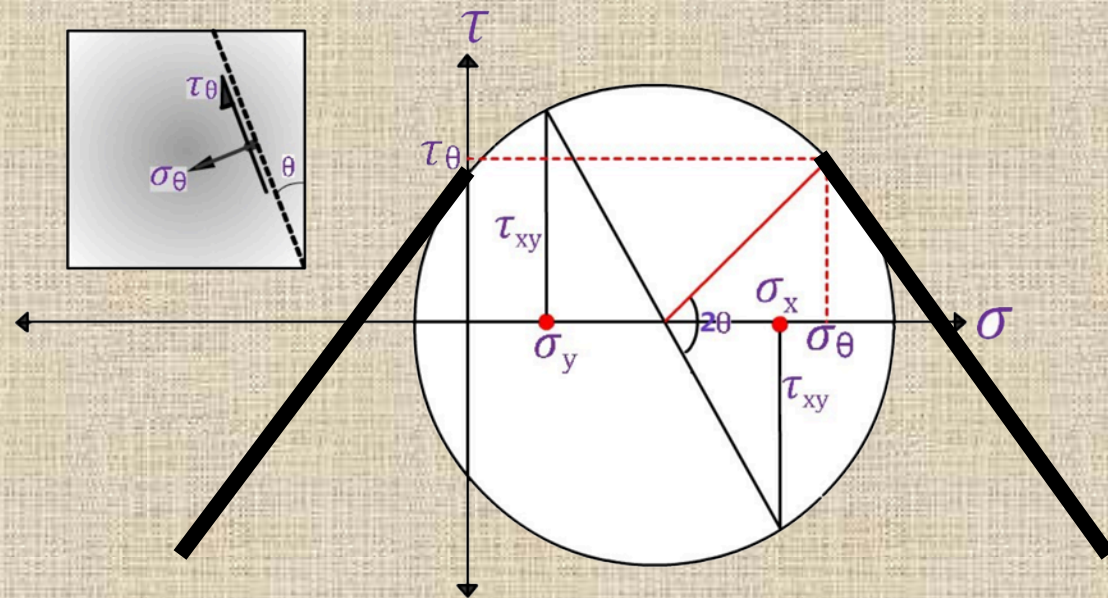


Web 101.84SM – Combined Stresses of Webs Going Over Rollers



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David Roisum, Ph.D.

Finishing Technologies, Inc.

Elementals

- Tension Variation - *Time*
 - imperfect drives
- Tension Variation - *MD*
 - Idler roller etc bearing drag
 - Idler roller etc inertia
- Tension Variation – *CD*
 - In-plane roller misalignment

- Baggy Webs – wrt *CD*

THICK WEBS ONLY:

Tension varies through the *thickness*

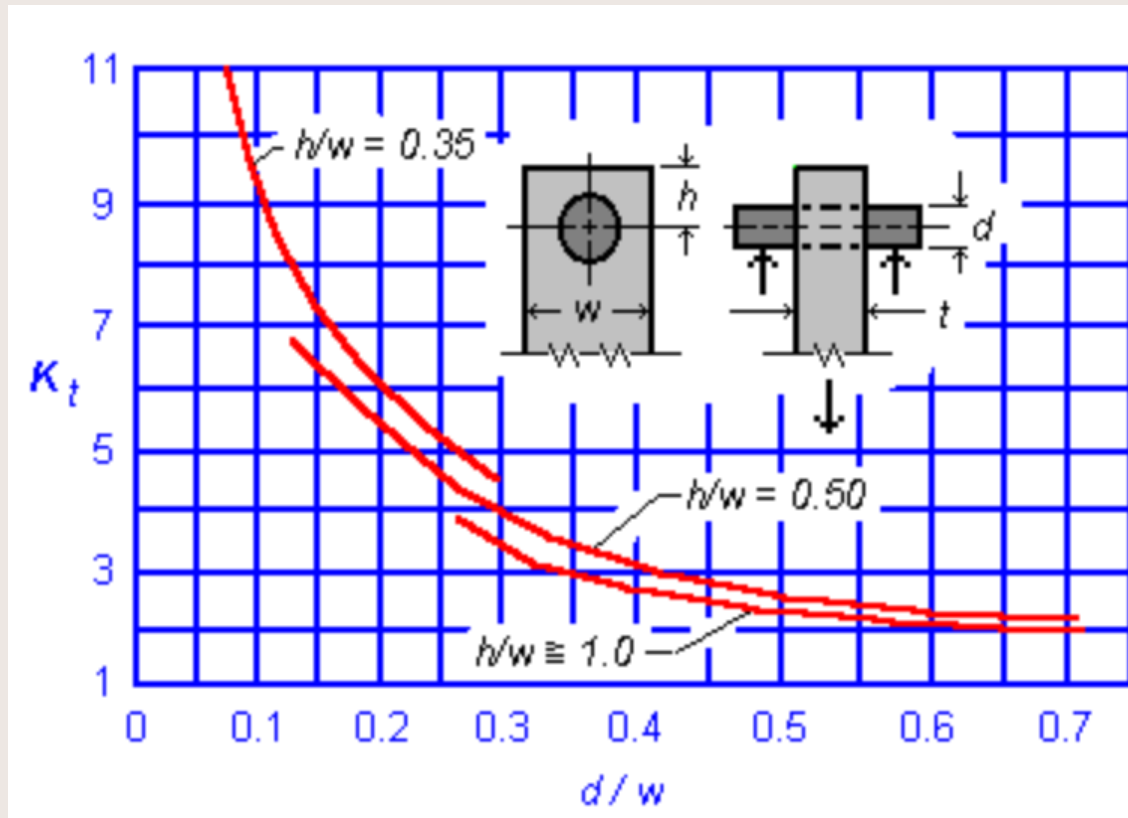
- Bend Radius
 - Wrap over rollers
- Curl
 - Residual stress

Simple and Safe

- (But not *over*-simplified to *only* 1 stress source)
- All major sources in **simple** one line equation
- Most variables **simple** to obtain
- Sources will be treated as **Stress Multipliers**
 - F_{TDE} etc
- Overall **Safety Factor** will be calculated
- CSR by AbbottApp makes this calculation simple

Stress Multiplier Model

- Tension on a specimen with a central hole



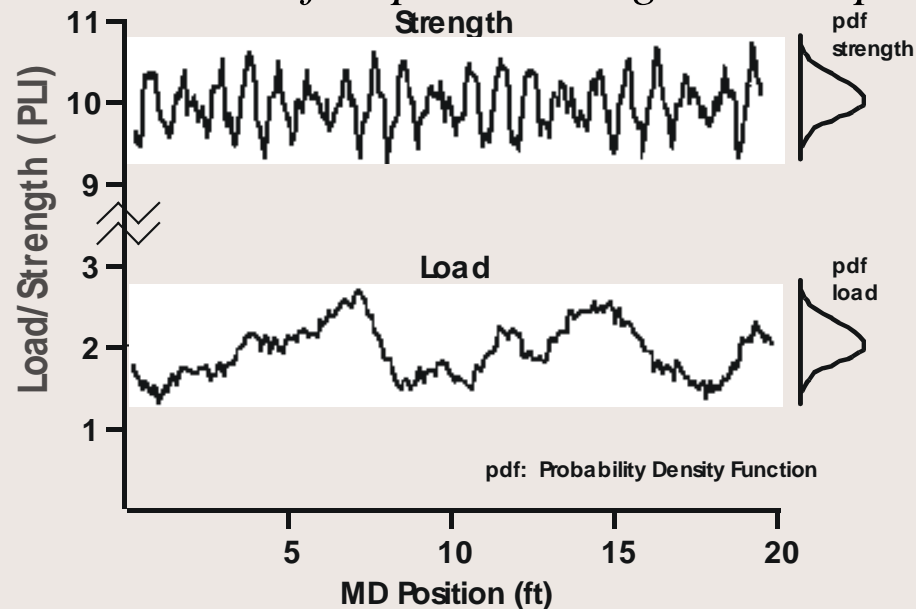
Tension Variations with Time

- Guidelines for average (across width) tension variations with time (F_{TDE}) at a given roller

< +/- 5% of setpoint during steady state

< +/- 10% of setpoint during speed changes

< +/- 50%? of setpoint during violent upsets



This example

$$F_{TDE} = 1.1$$

Could be written into performance spec in purchasing contract

Web Machine

Buying Guide

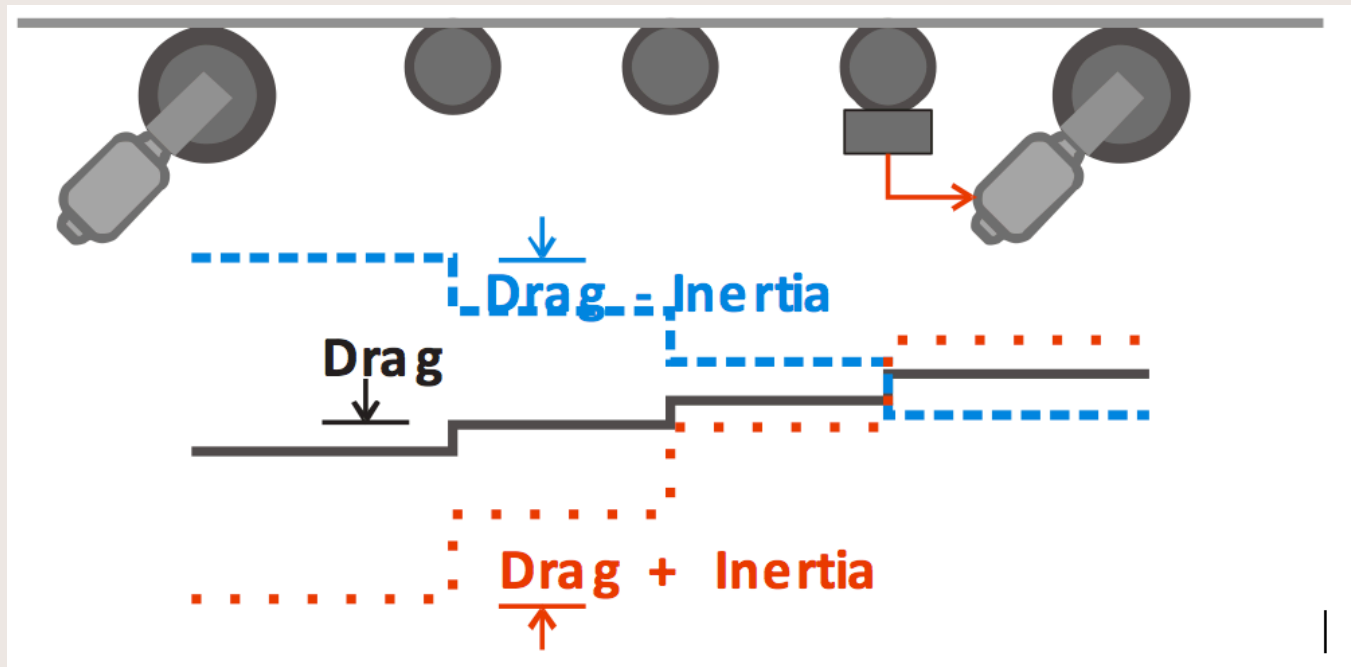
DR Roisum

Destech & TAPPI

Tension Variations with MD

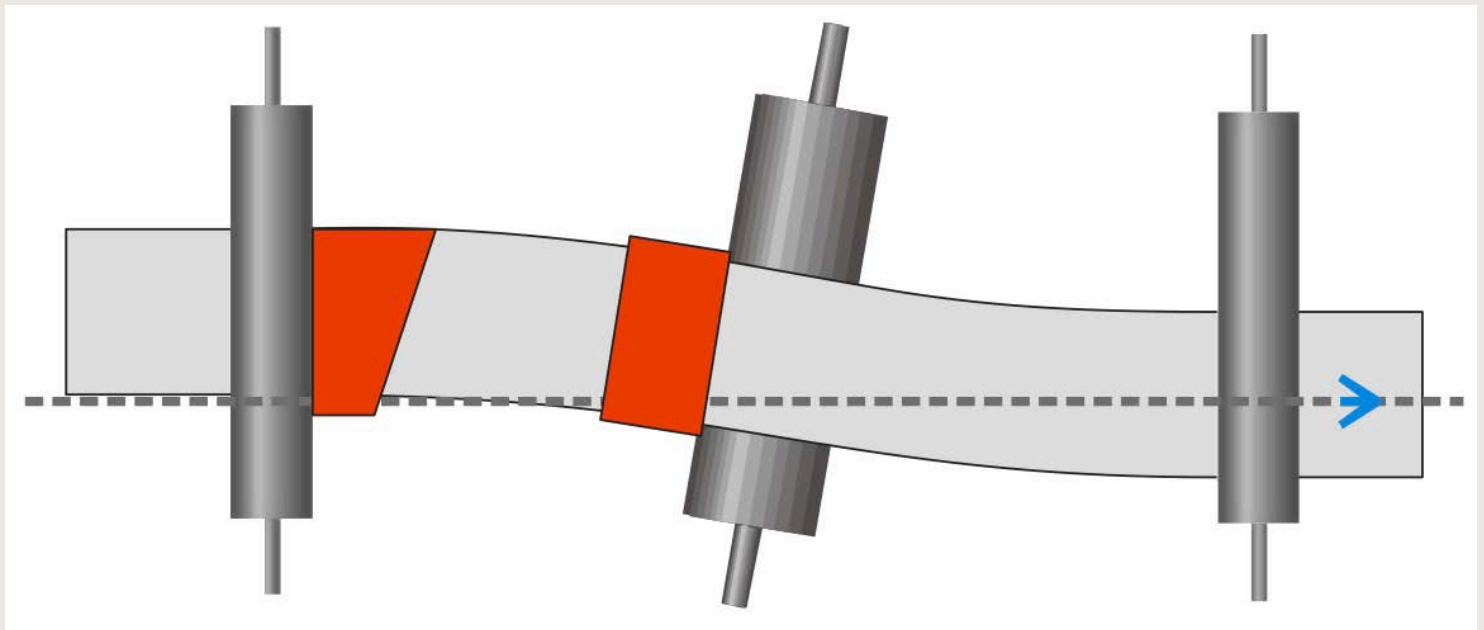
- Guidelines for average (across width) tension rise in a drive zone (F_{TDM})
< 10% of setpoint

This example $F_{TDM} = 1.1$



Tension Variations in CD

- Guidelines for tension variations across width due to **inplane roller misalignment (F_M)**
< slack web on inside of curve or 2 X average on outside



Slack Web Calculation

- Using guiding theory (Shelton, 1965) we can calculate the multiplication factor (w.r.t. stress riser on outside of bend) as

$$F_M = 1 + \frac{\theta_i}{\epsilon_T \frac{L}{W}}$$

Where

θ = misalignment angle

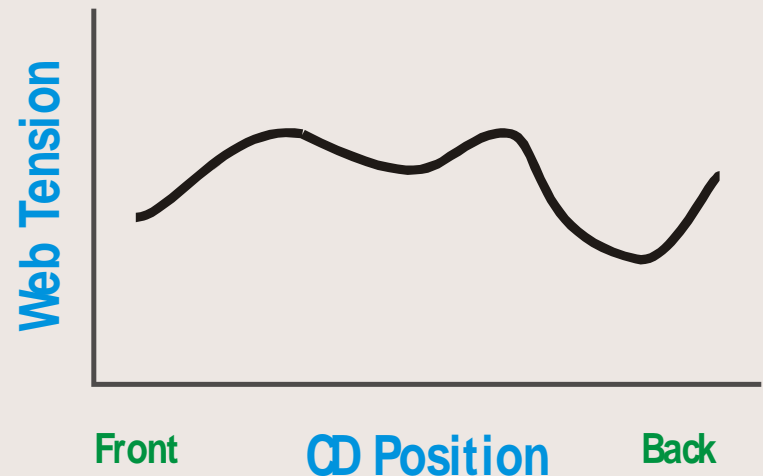
ϵ_T = strain due to tension

L = length of span

W = width of span

Baggy Webs

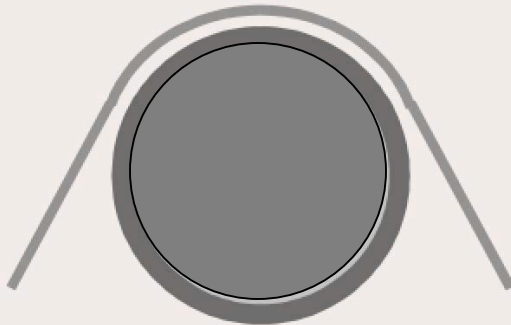
- We will give the stress multiplier due to bagginess as F_B



Bend Radius On Rollers

- Only a concern for thick webs
- We calculate strain multiplier as

$$\epsilon_{RBR} = \frac{\text{half thickness}}{\text{radius of curvature}} = \frac{t}{D}$$



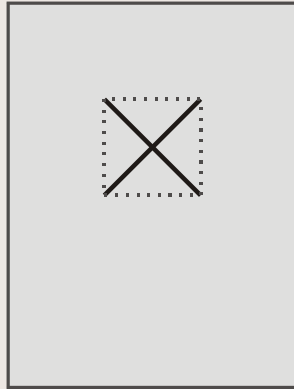
Curl

- Only a concern for thick webs
- We calculate strain multiplier from measured curl radius as

$$\epsilon_c = \frac{t}{2r_c}$$

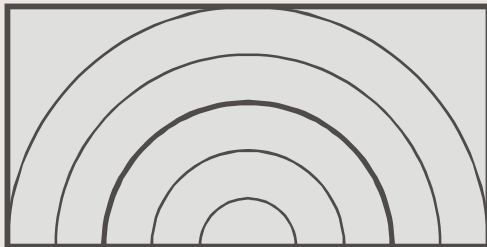
Curl Measurement

- X Cut

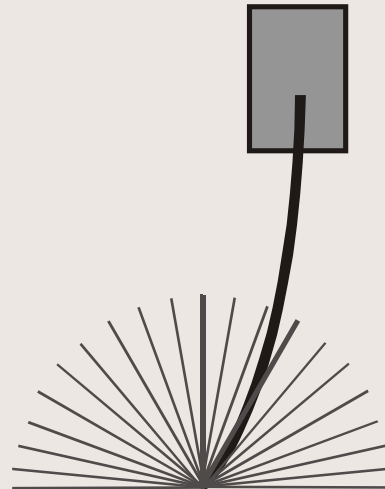


Swanson, Ron. *Measurement of Web Curl*. AIMCAL Web Handling Conf., Charlotte, May 7-10, 2006

- Radius Template



- Hanging Angle



Summary Safety Factor

- 0) Check that all components are in **MD**
 - 1) Check that all components *could* align in **space**
 - 2) Check that all components *could* align in **time**
- Ultimate Safety Factor considering all

c

$$SF = \frac{\sigma_Y}{E_1 [F_B F_M F_T D E F_{TDM} (\epsilon_T + \epsilon_C + \epsilon_{RBR})]}$$

Applications

- First calculate a Safety Factor for a known marginal application.
- Then one could allocate a precision budget in different ways. Examples.
 - Difficult drives might demand more precise alignment in compensation
 - Baggy webs might demand more precise mechanicals and controls to not go over ‘budget’
 - While you still will not be allowed to run crappy web on a crappy machine, you will at least know what you need to change

Generalizations

<u>Tmax</u> <u>Tyield</u>	<u>Sfmin</u>	<u>Industry</u>	<u>Major Variations / Concerns</u>
4	3	Paper	Mild bagginess / web breaks
2	1.5	Tissue	Extreme bagginess / loss of crepe
5	2-3	Film convert	Bagginess, misalign / many
4-5	??	Yours	Your mileage may vary

Limitations & Future Work

- Slightly conservative because it assumes worst case *alignment* of contributions
- Anisotropic considerations are minor
- Linearity (because we used *superposition*):
- Contributions singly or in combination can not be so severe as to cause a *slack web*
- Still, SIB (Simple Is Best)

Questions?

Answers:

David Roisum, Ph.D.

<http://www.webhandlingblog.com/>

<http://www.roisum.com>

drroisum@aol.com

920-312-8466 cell

